



Use of HART-II Measured Motion in CFD

D. Douglas (Doug) Boyd, Jr.

Aeroacoustics Branch

NASA Langley Research Center

Hampton, VA 23681

HART-II Workshop, April 28, 2008

Montréal, Canada



Outline

- Introduction
- Implementation of measured motion
- Predictions using measured motion
- Predictions using measured motion vs.
Predictions using coupled motion (still in work)
- Summary

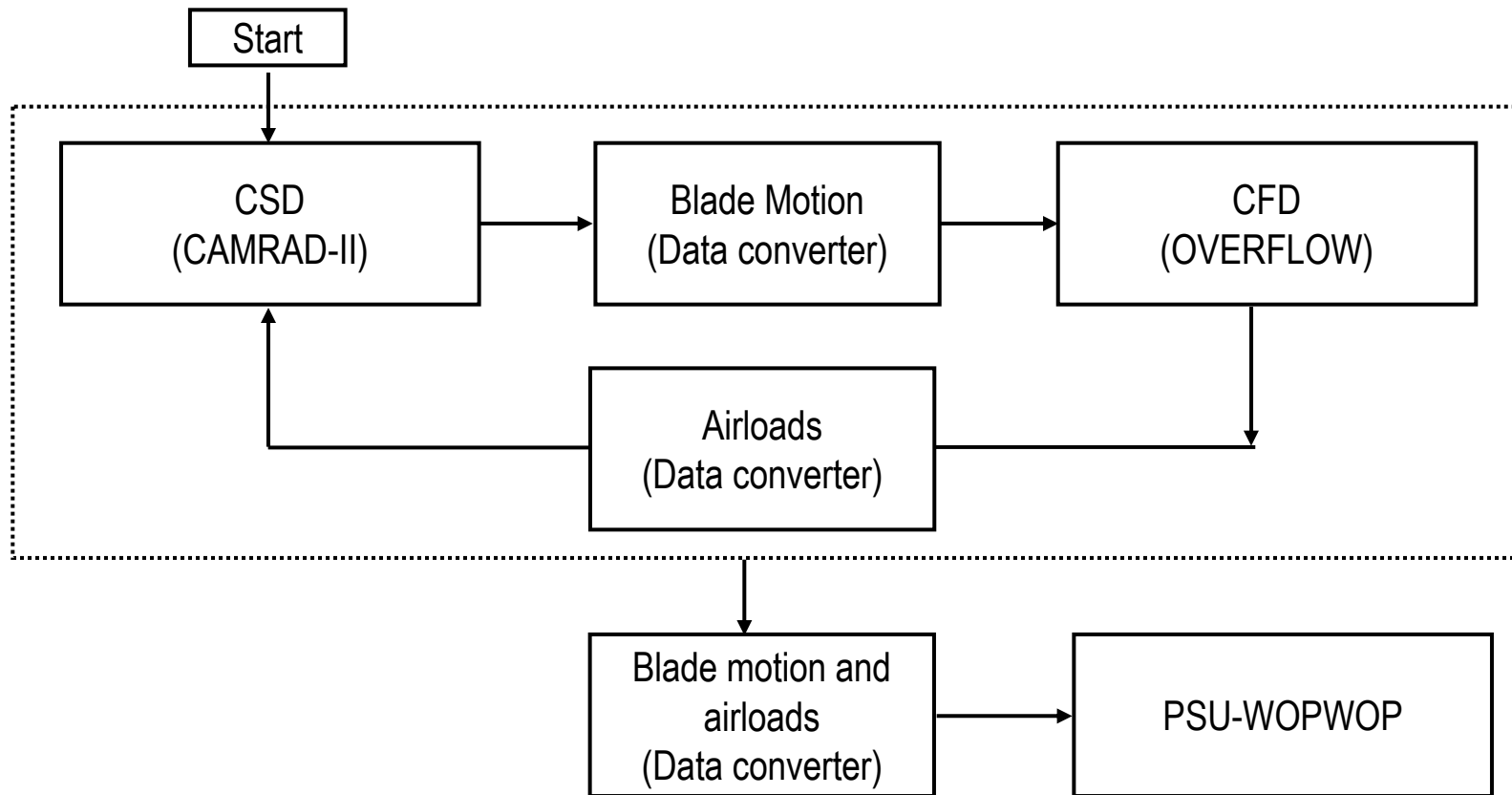


Introduction

- Historically, comprehensive analyses used for input to acoustic calcs...
- Historical analyses focused on: Lifting line aerodynamics + beam models
 - Beam models have evolved into finite beam models (or higher)
 - Ability to model more general blade configurations
 - Lifting line aerodynamics still used, predominantly.
 - Assumptions often violated
- Need to evolve lifting line aerodynamics to 1st principles.
 - CFD instead of lifting line
- Current analyses focused on: CFD + CSD coupling
 - Beam models still very good (CSD typically from comprehensive analysis)
 - Generally, CFD replaces aerodynamics in comprehensive analysis.
 - BUT, Need a way to examine both pieces individually...



(Loosely) Coupled CFD/CSD Methods



NOTE: It can be hard to decipher which piece is a problem, if one occurs.

- Reads OVERFLOW outputs
- Generates loading file
- Generates patch file
- Includes elastic motion



Dissection of Coupled Method

Goal: Try to examine each piece of method in isolation.

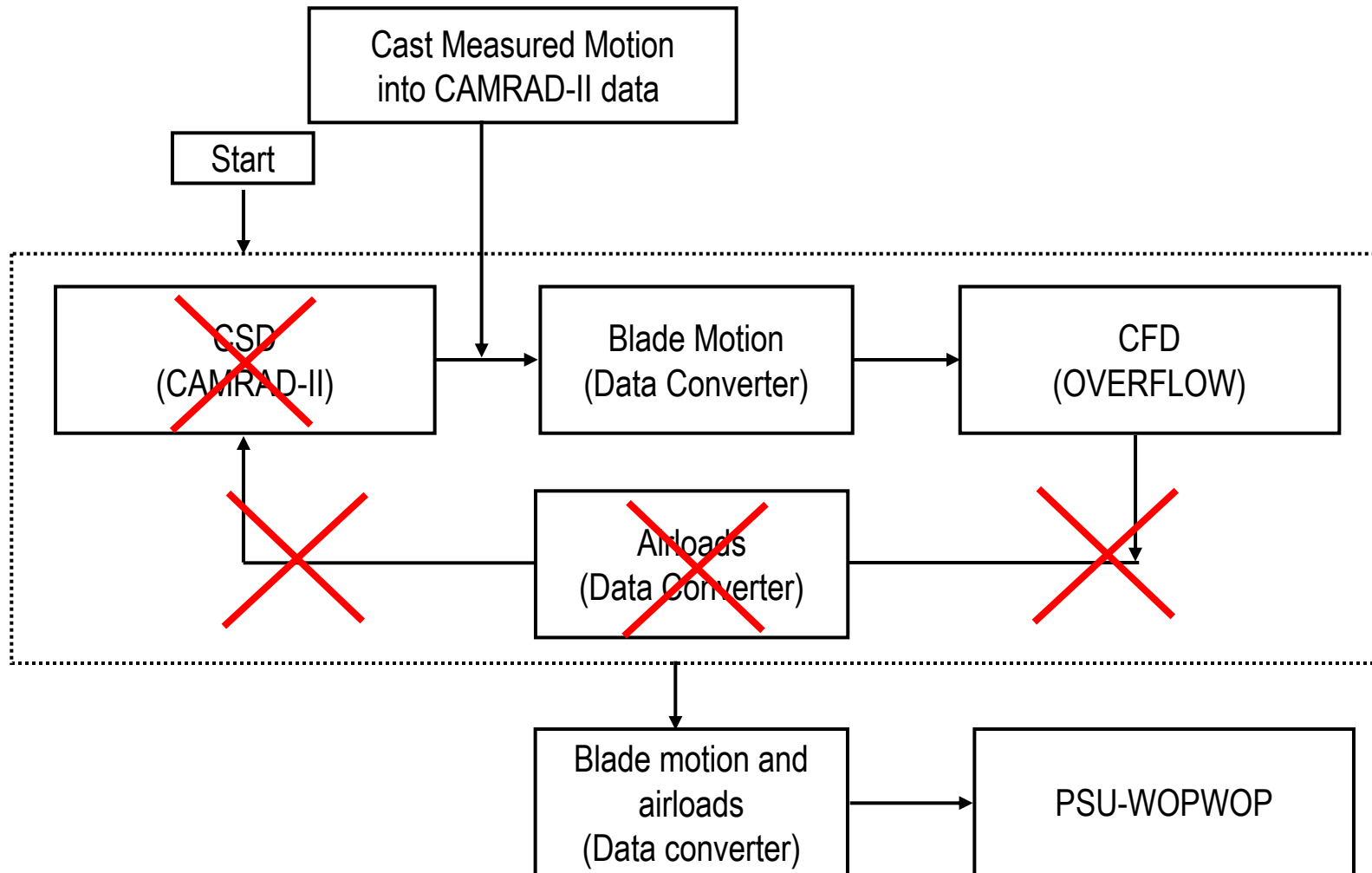
Why: If successful, this should help understanding of each component.

- Step 1: Isolate CFD method using measured blade motion.
 - Ideally, this should generate “correct” airloads, noise, etc.
 - Assumes all blades are periodic AND are identical in motion.

- Step 2: Isolate CSD with “correct” airloads from Step 1 above.
 - Ideally, this should generate “correct” blade motions.
 - (Not being done yet... still working on Step 1)...



Step 1: Isolate CFD method.





Measured Motion to CAMRAD-II data

- Need 3 displacements and 3 rotations at each location.
- Measured elastic data only contains 2 displacements and 1 rotation...
 - Must assume something for missing data.
- CFD grid already includes 2.5° pre-cone and built-in twist.
- Θ_0 , Θ_{1c} , Θ_{1s} , Θ_{3P-HHC} are measured quantities also.



Measured Motion to CAMRAD-II data (cont)

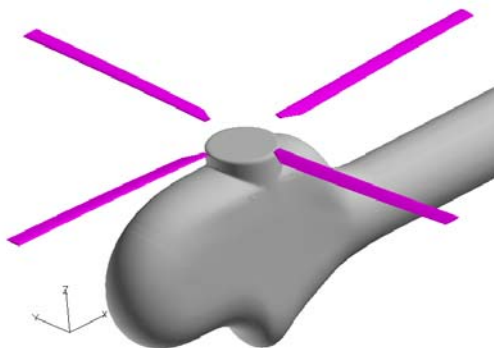
- Linear displacement of each location :
 - Flap = measured local elastic flap
 - Lag = measured local elastic lag
 - Extension = 0.0 (ASSUMPTION)

- Angular rotation of each location :
 - Flap = \tan^{-1} (local flap deflection / r) (ASSUMPTION)
 - Lag = \tan^{-1} (local lag deflection / r) (ASSUMPTION)
 - Pitch = $\Theta_0 + \Theta_{1c} + \Theta_{1s} + \Theta_{3P-HHC}$ + measured local elastic torsion

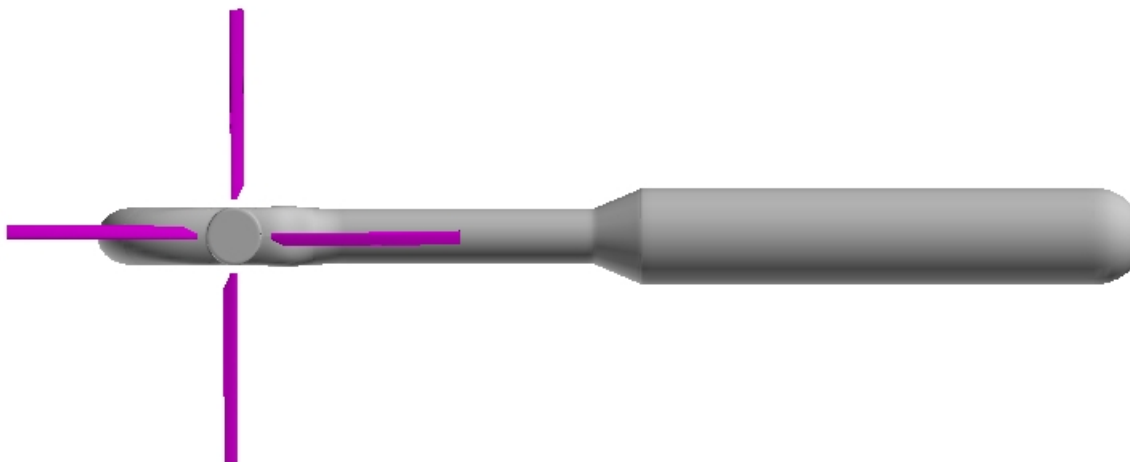
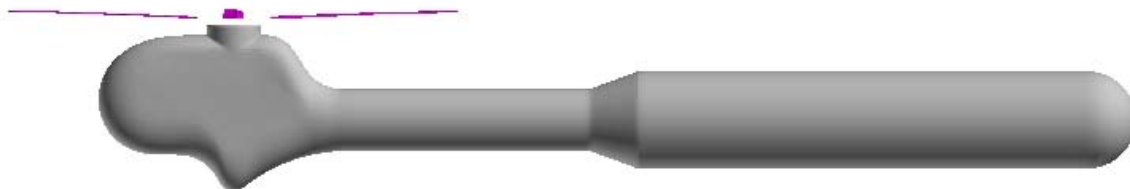
- These quantities are reconstructed using formulae and data in van der Wall document...
- All measured quantities are from Blade-1 data.
- This motion is then used as if it had come from CAMRAD-II...



Grid Configuration



- Blade: (3 grids each)
 - main: 273 x 113 x 33
 - tip: 158 x 48 x 33
 - root: 68 x 66 x 33
 - Sting: (15 grids)
 - 630,861 points
 - Background: (76 grids)
 - Pringle grids: (3 per blade)
-
- Level 1 spacing = 0.10c
 - First off body point... $y^+ < 1.0$
 - Total grid points = 68,171,477



- Isolated rotor: identical to full configuration, but...
- Do not include sting grids...
- Level-1 specified “bricks” are same in both configurations.



Results with Measured Motion:

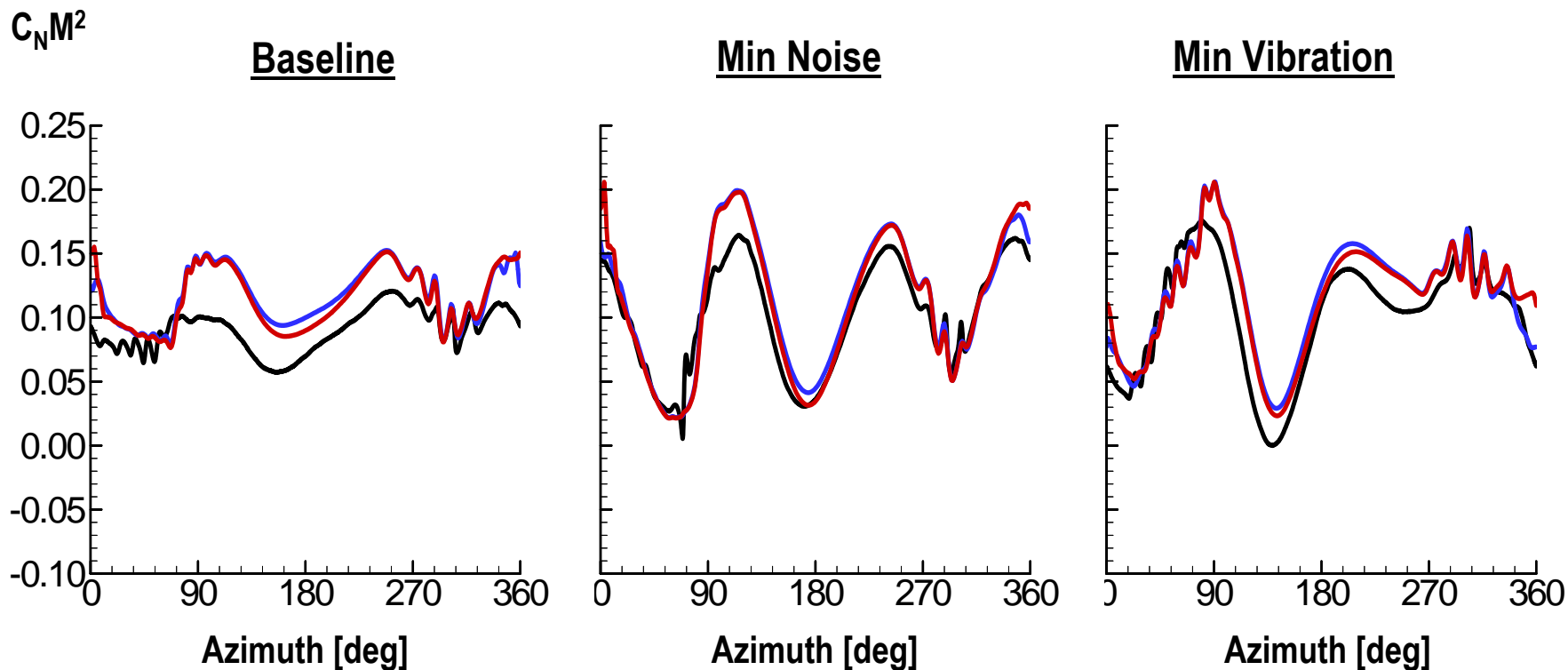
- **Isolated Rotor**
- **Full Configuration**



$C_N M^2$ Predicted with Measured Motion

OVERFLOW + measured motion

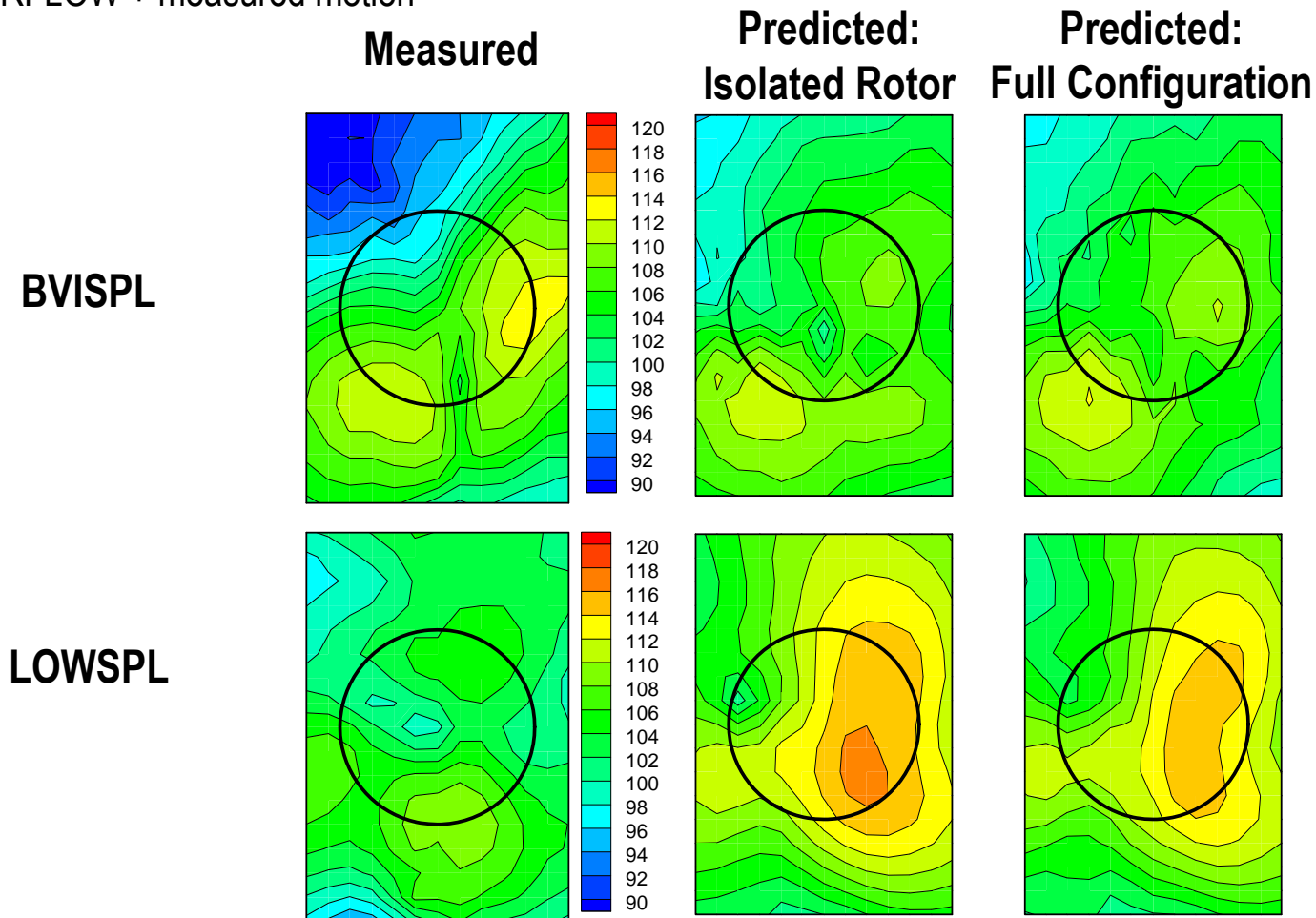
— Measured
— Predicted: Isolated Rotor
— Predicted: Full Configuration





Baseline: Using Measured Motion

OVERFLOW + measured motion





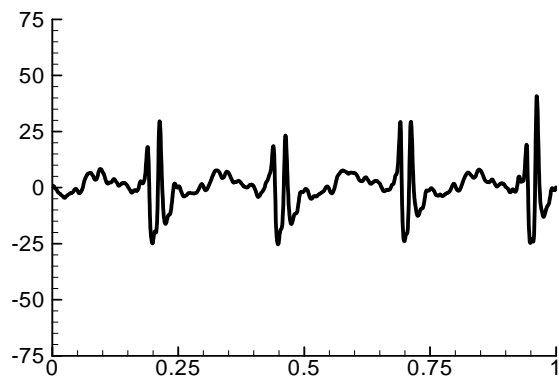
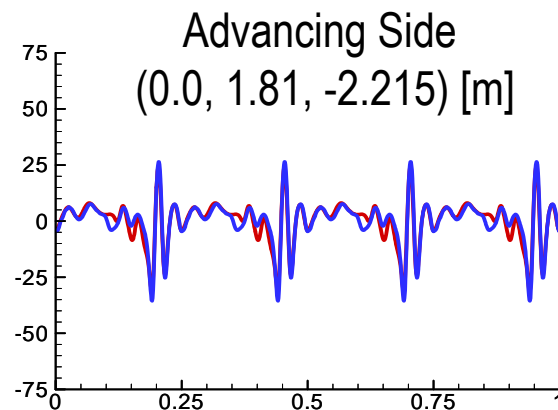
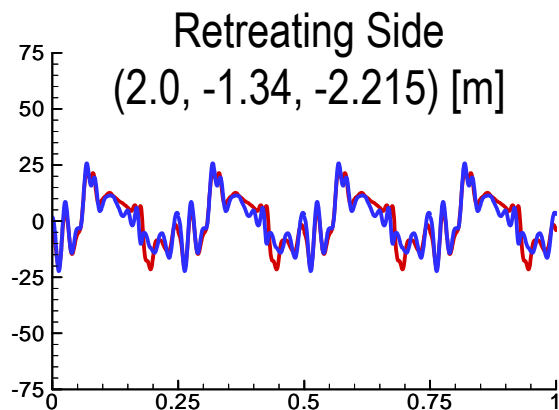
Baseline: Using Measured Motion

Acoustic Pressure Time Histories [Pa]

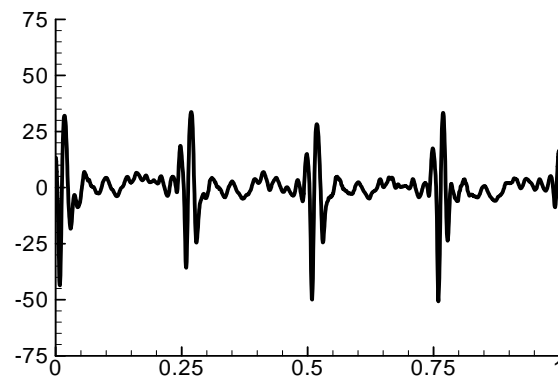
OVERFLOW + measured motion

— Measured
— Predicted: Isolated Rotor
— Predicted: Full Configuration

Acoustic
Pressure
[Pa]



Fraction of Revolution

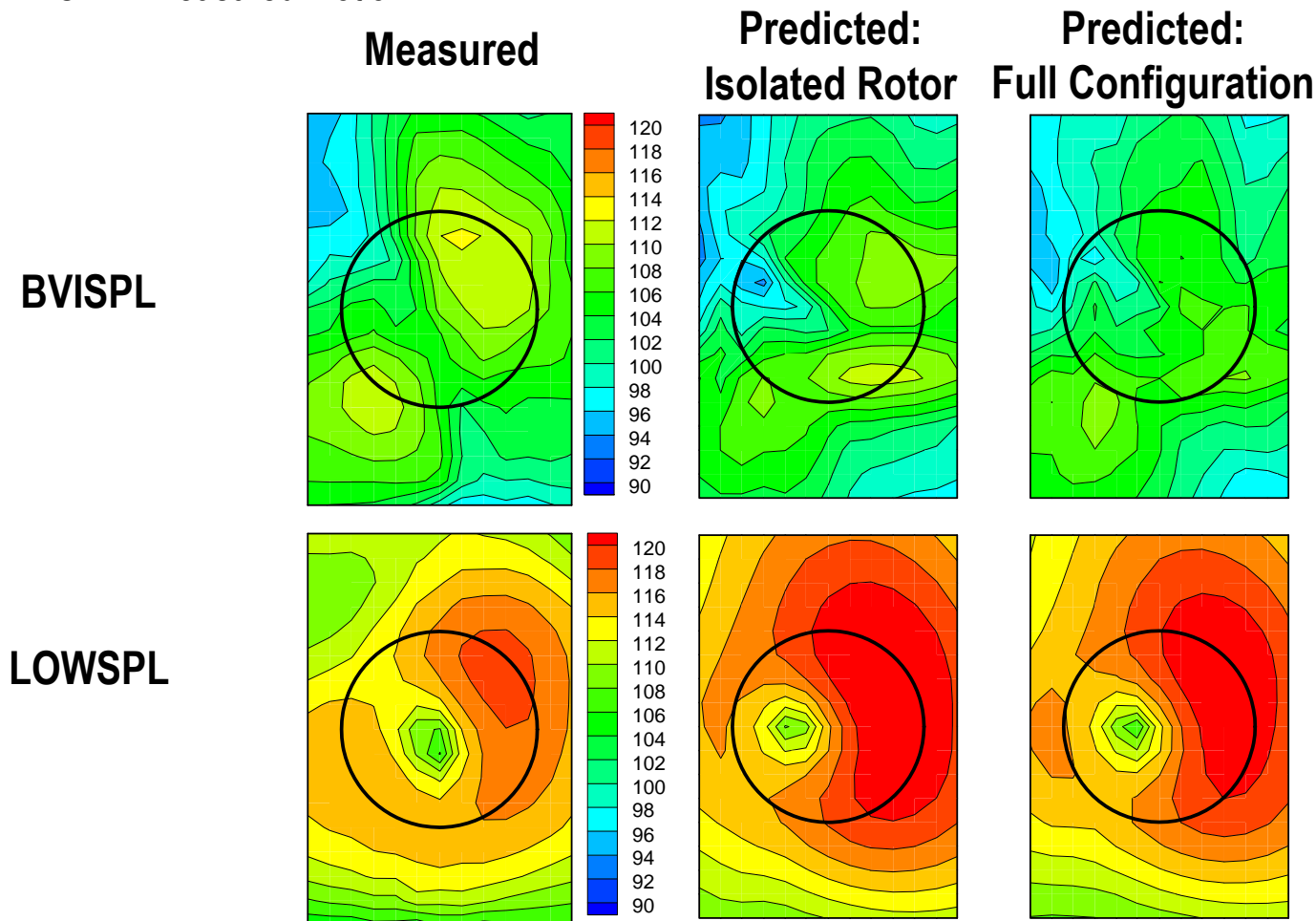


Fraction of Revolution



Min Noise: Using Measured Motion

OVERFLOW + measured motion





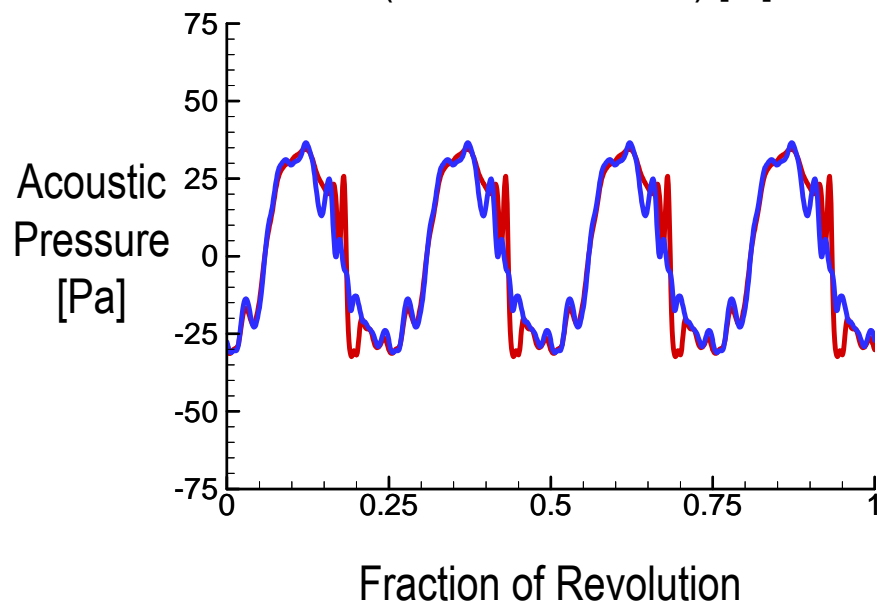
Min Noise: Using Measured Motion

Acoustic Pressure Time Histories [Pa]

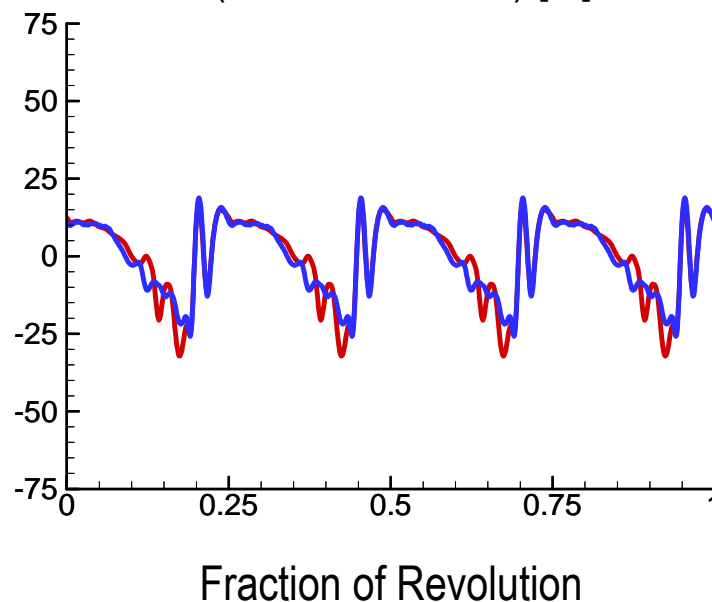
OVERFLOW + measured motion

— Predicted: Isolated Rotor
— Predicted: Full Configuration

Retreating Side
(2.0, -1.34, -2.215) [m]



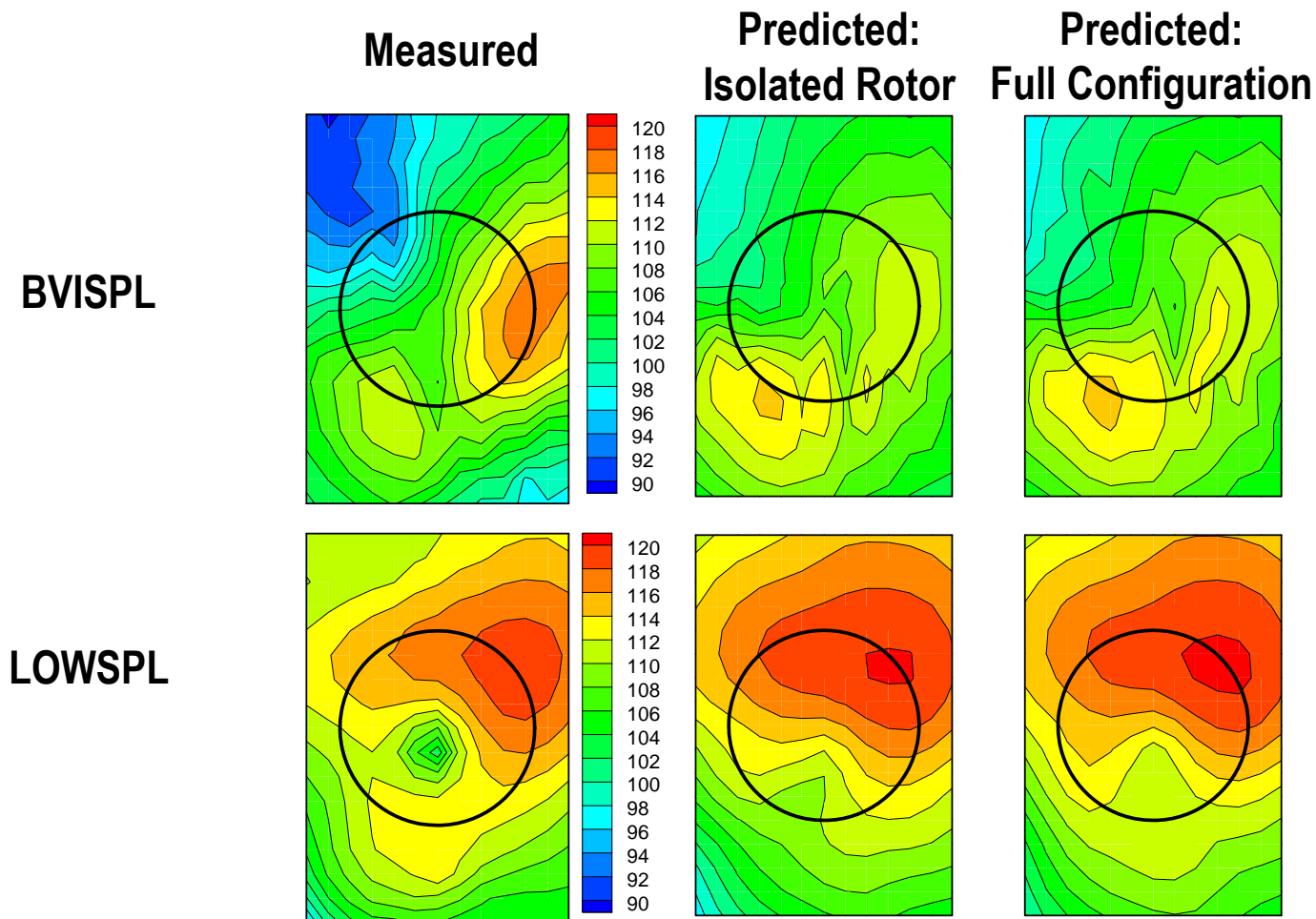
Advancing Side
(0.0, 1.81, -2.215) [m]





Min Vib: Using Measured Motion

OVERFLOW + measured motion





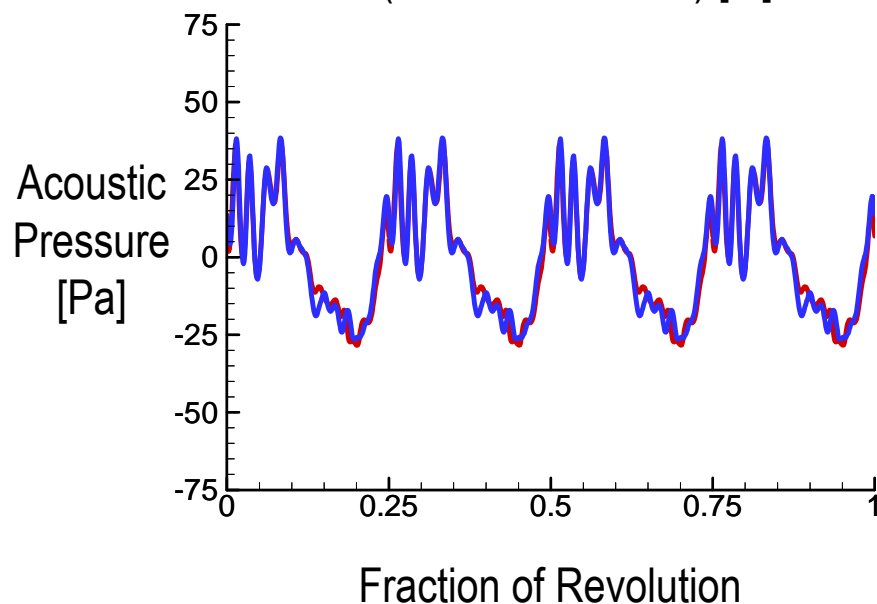
Min Vib: Using Measured Motion

Acoustic Pressure Time Histories [Pa]

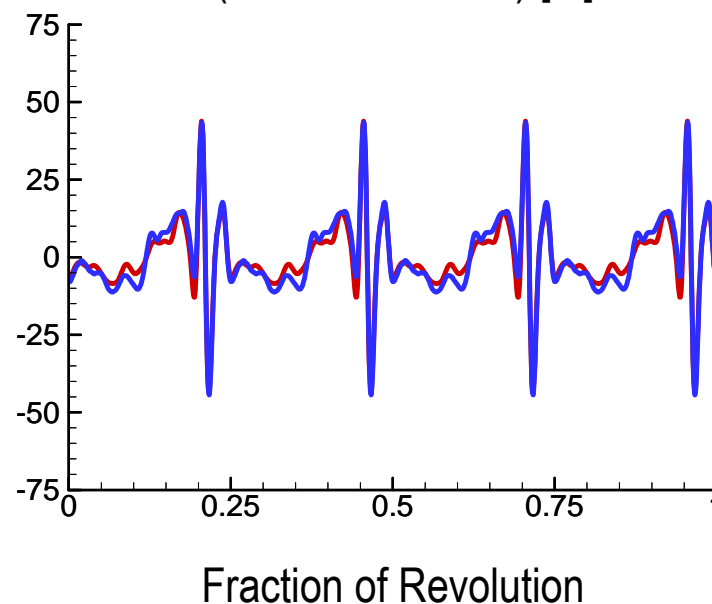
OVERFLOW + measured motion

— Predicted: Isolated Rotor
— Predicted: Full Configuration

Retreating Side
(2.0, -1.34, -2.215) [m]



Advancing Side
(0.0, 1.81, -2.215) [m]





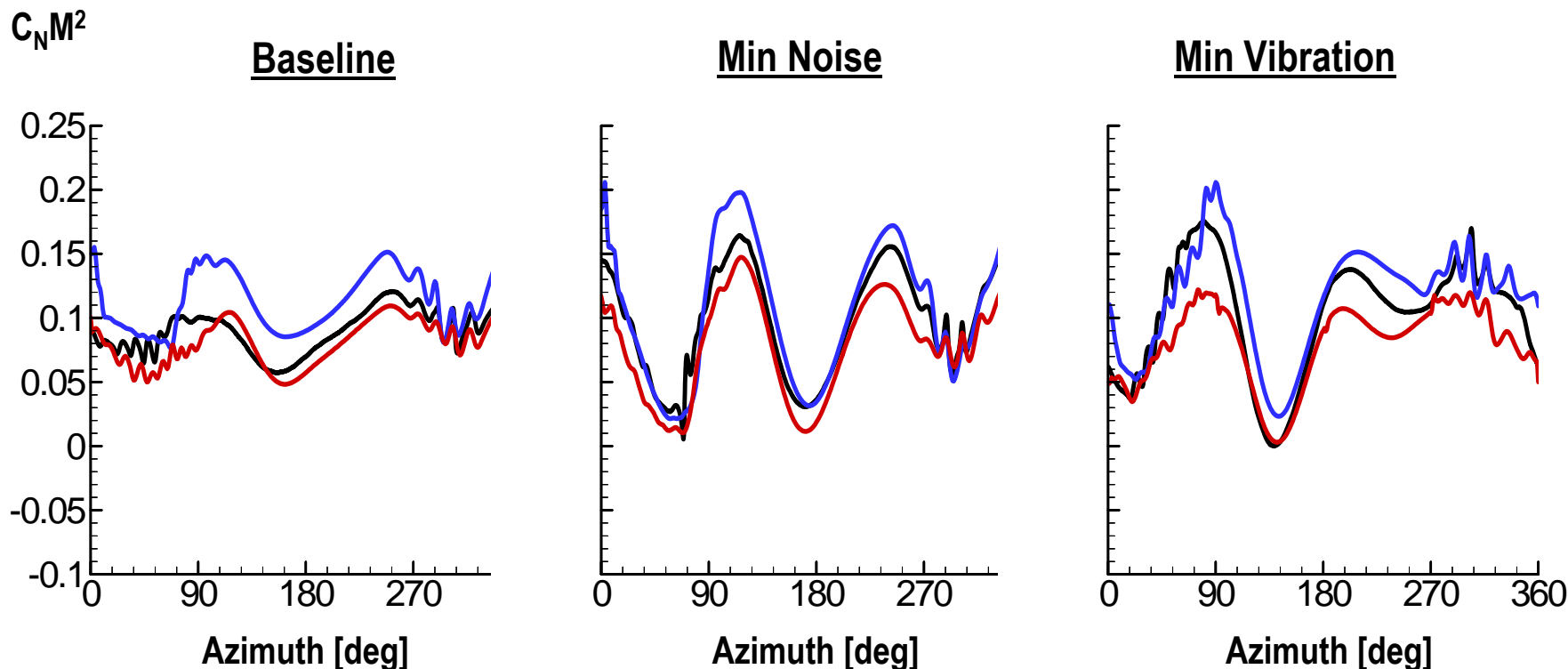
Full Configuration: Measured Motion vs. Coupled Motion



$C_N M^2$: Measured Motion vs. Coupled

Full Configuration

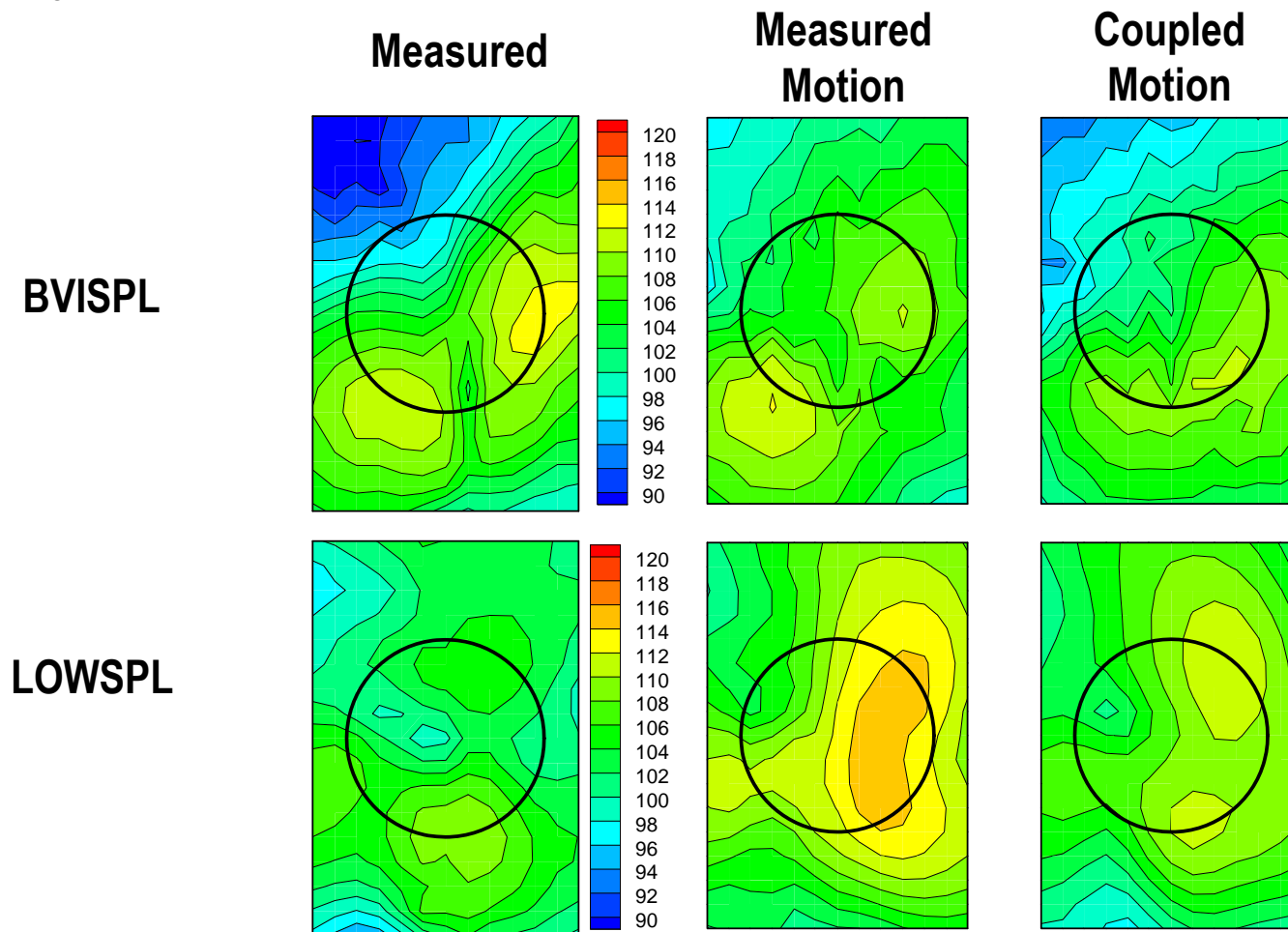
— Measured
— Predicted: With Coupled Motion
— Predicted: With Measured Motion





Baseline

Full Configuration





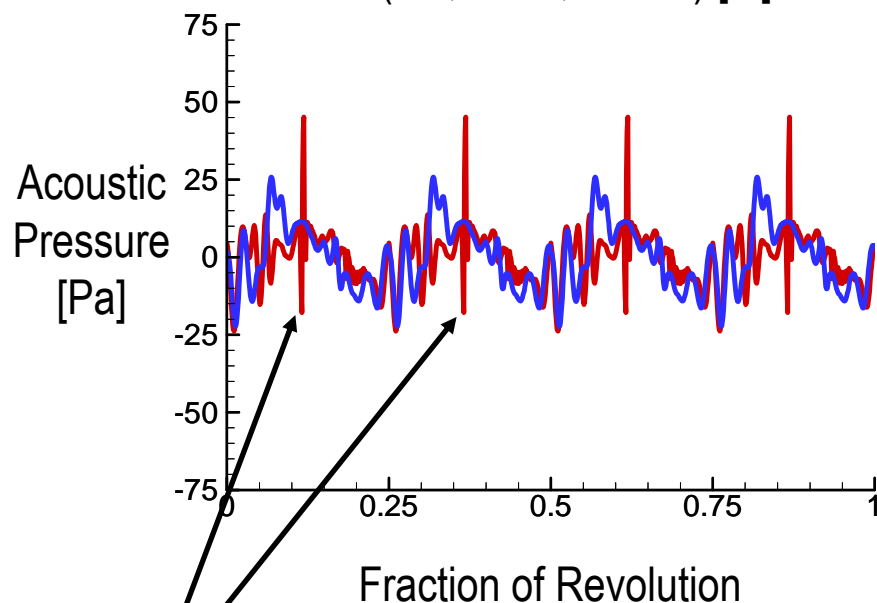
Baseline: Meas. Motion vs Coupled Motion

Acoustic Pressure Time Histories [Pa]

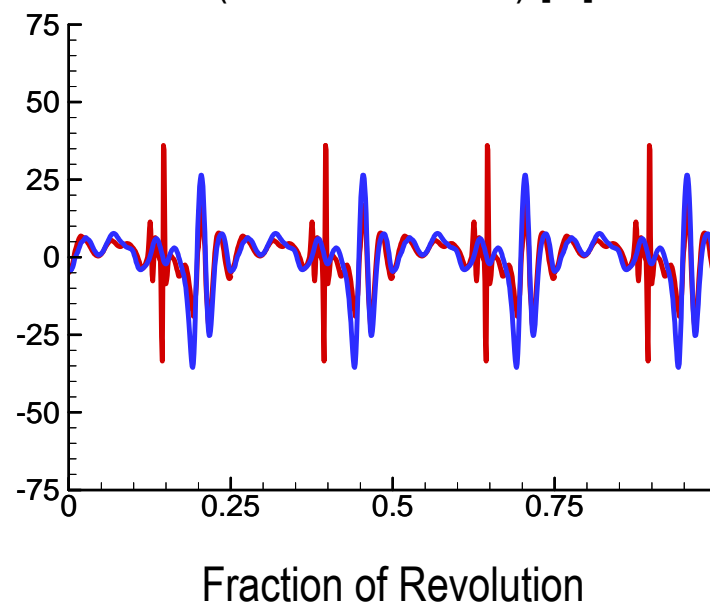
Full Configuration

— Predicted: Coupled Motion
— Predicted: Measured Motion

Retreating Side
(2.0, -1.34, -2.215) [m]



Advancing Side
(0.0, 1.81, -2.215) [m]

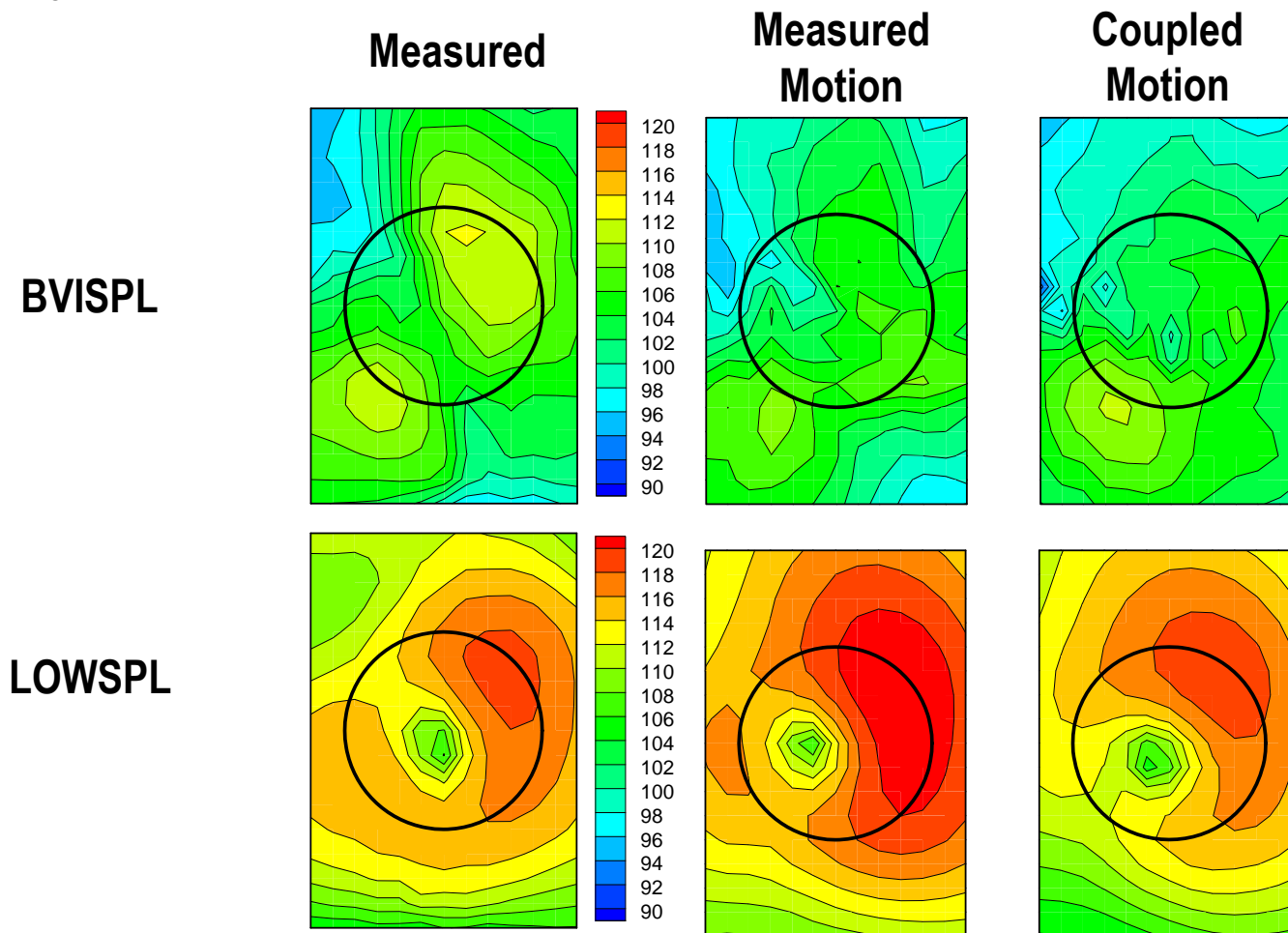


Frequencies are > 40 BPF:
Do not contribute to contours on previous slide.



Min-Noise Case

Full Configuration





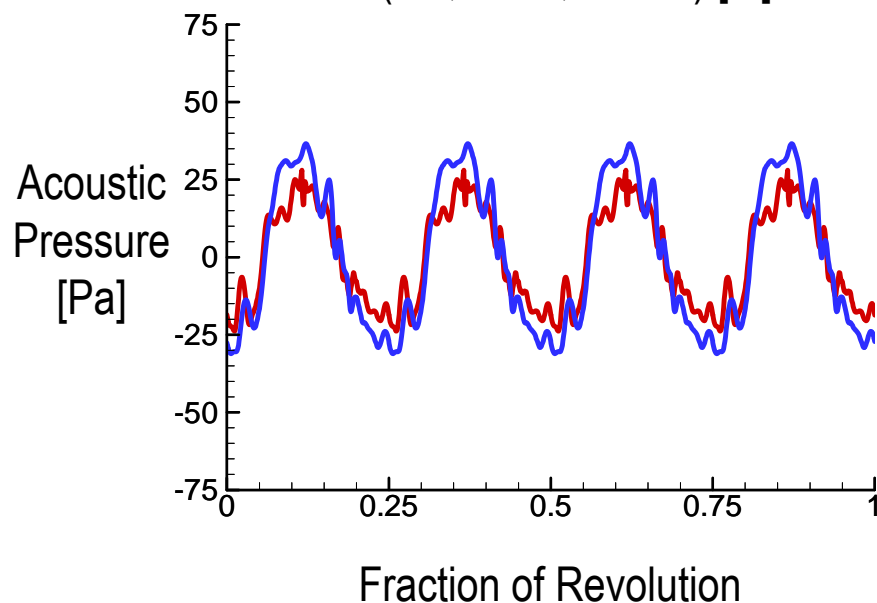
Min Noise: Meas. Motion vs Coupled Motion

Acoustic Pressure Time Histories [Pa]

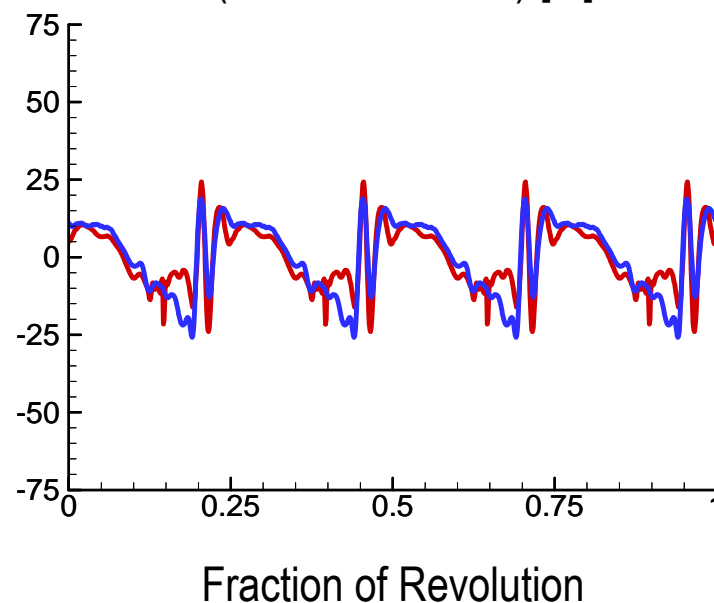
OVERFLOW + measured motion

— Predicted: Isolated Rotor
— Predicted: Full Configuration

Retreating Side
(2.0, -1.34, -2.215) [m]



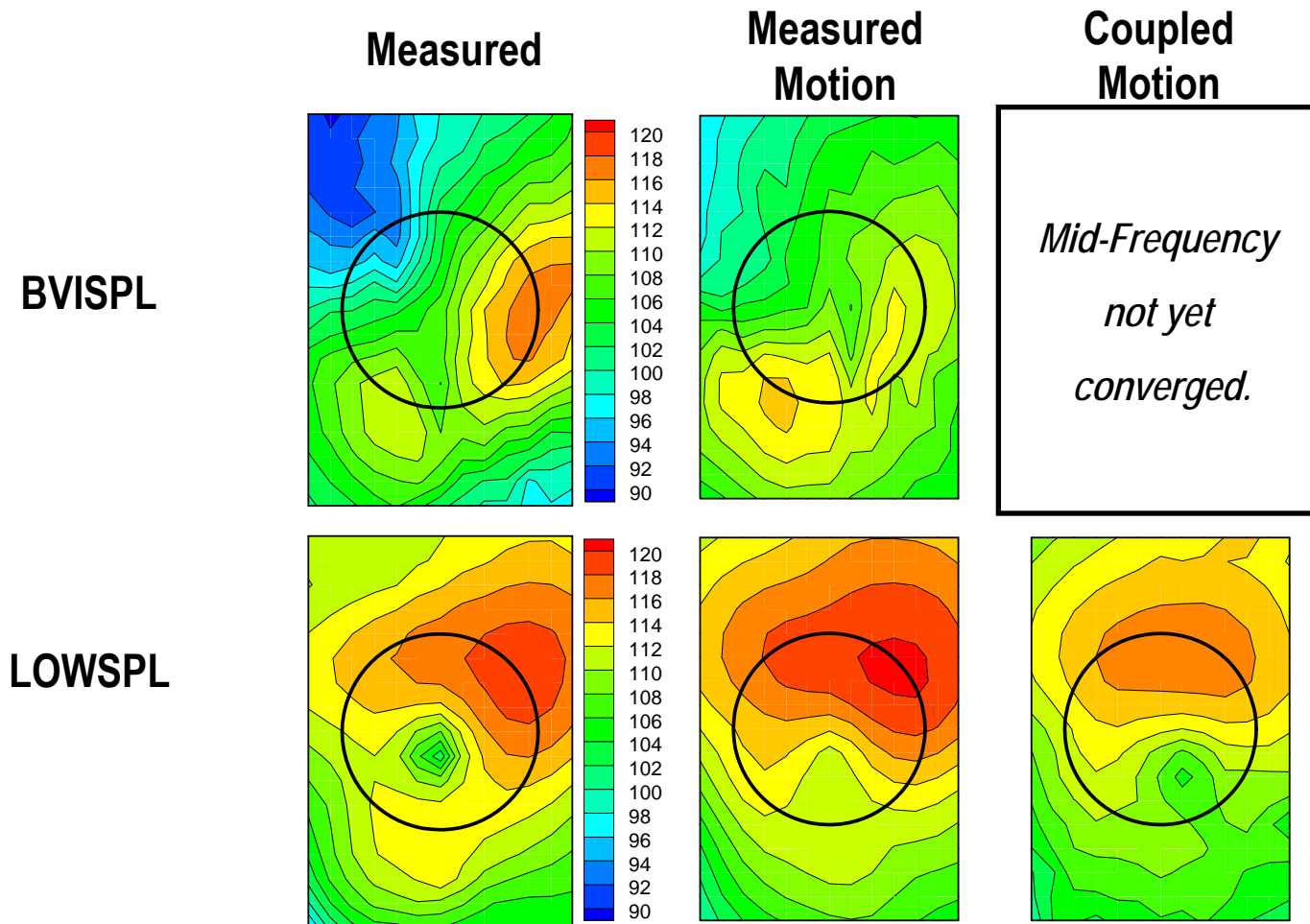
Advancing Side
(0.0, 1.81, -2.215) [m]





Min-Vibration Case

Full Configuration



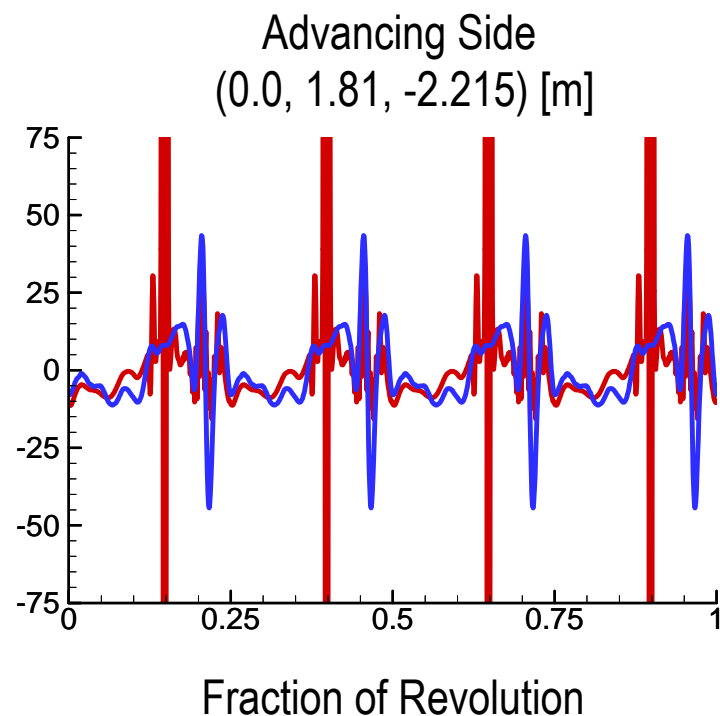
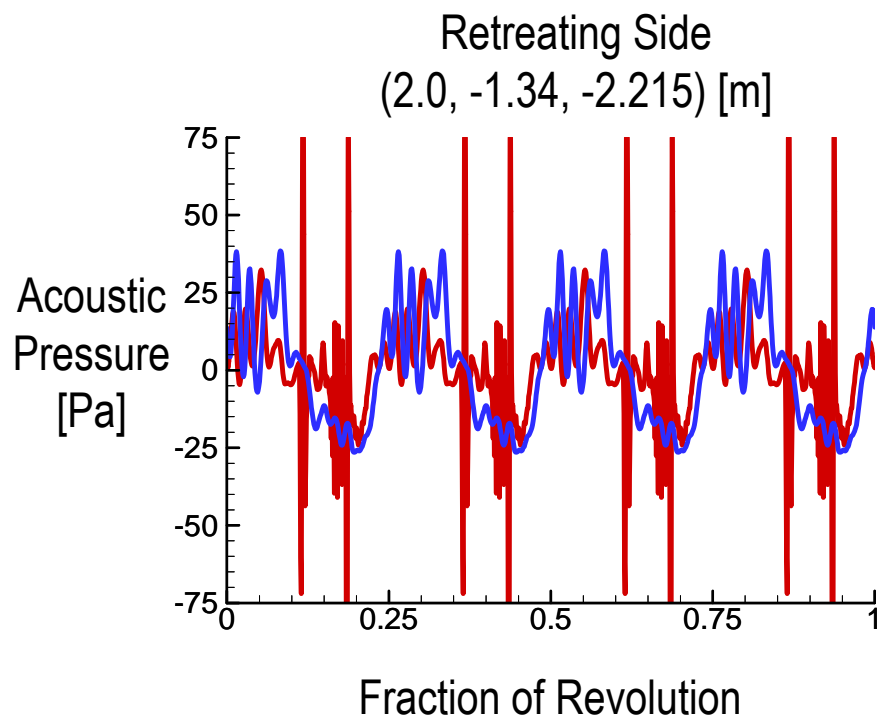


Min Vib: Meas. Motion vs Coupled Motion (Not converged yet)

Acoustic Pressure Time Histories [Pa]

OVERFLOW + measured motion

— Predicted: Isolated Rotor
— Predicted: Full Configuration



Low frequency components are "converged"... see CNM2 plots.
Mid & High frequency content are not yet converged.



Summary

- Work is still in progress.
- Using measured motion in CFD:
 - Temporary by-pass of CSD to (hopefully) aid understanding.
 - Why is thrust is so high with the measure data?
 - Blade 1 vs Blade 2, 3, 4 ?
- MV coupled motion case not yet converged.
- Next will be “Step 2”: Put predicted airloads back into CSD code.
- Work is being documented into a NASA report.

Wish list:

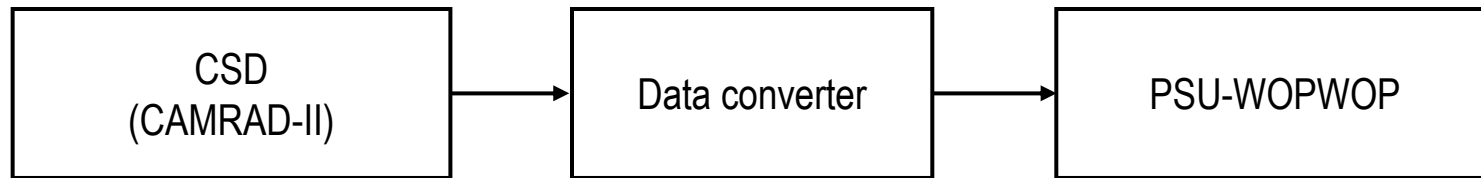
1. Measured acoustic pressure time histories for MN and MV cases.
2. Surface pressures (at $r/R=0.87$)
3. Impedance properties of sting foam.



Backup slides



Historical Prediction Methods



- Comprehensive Analysis
- Trim to Thrust and Hub Moments
- Lifting Line aerodynamics
- Blade dynamics

- Reads CAMRAD-II output
- Generates loading/function file
- Generates patch file
- Generates namelist input file
- Assumes rigid blade motion

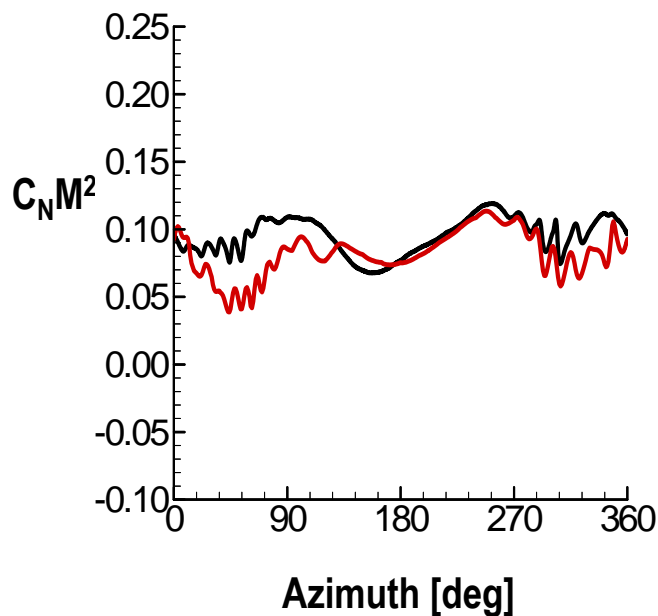
- Tone noise prediction
- Time domain calculation
- Outputs acoustic pressure
- Also, outputs SPL information



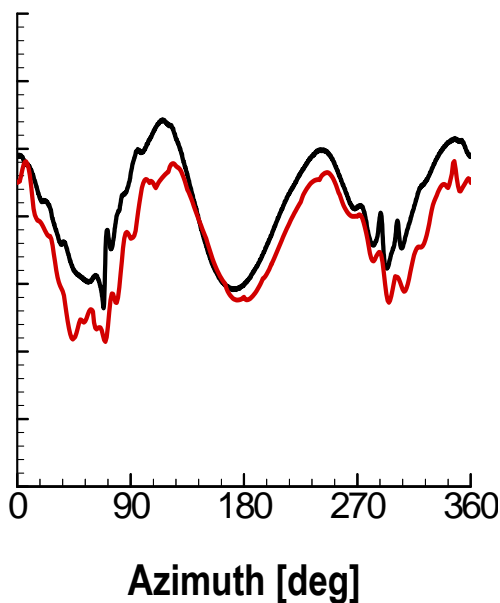
Historical Methods Example: $C_N M^2$

— Measured
— Predicted

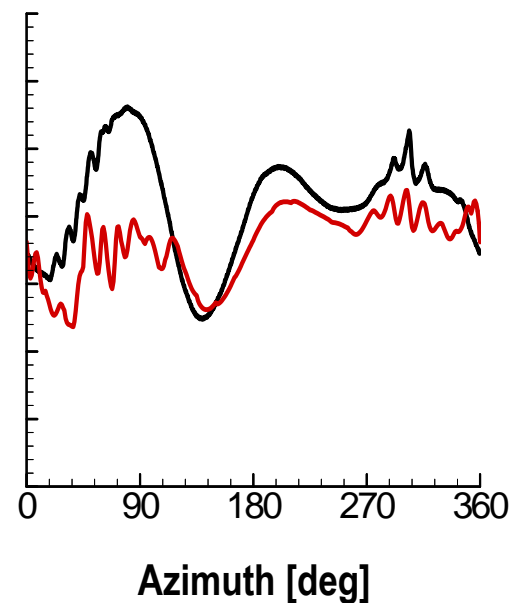
Baseline



Min Noise



Min Vibration

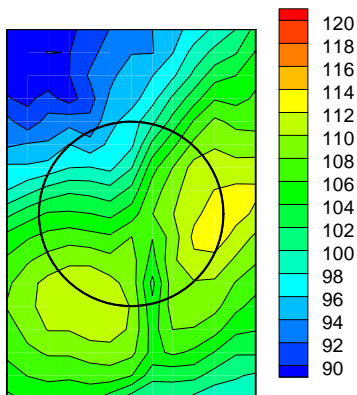




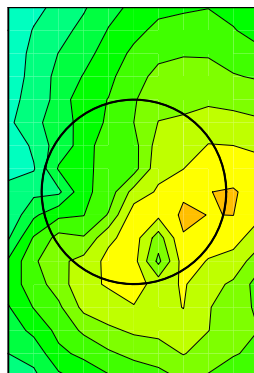
Previous Methods: BVI Directivity

Baseline

Measured

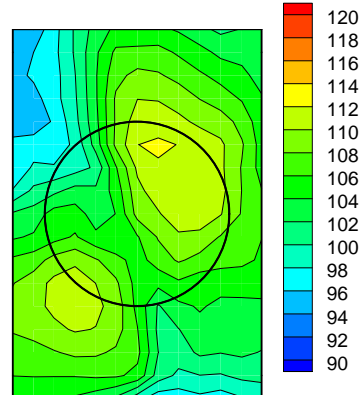


Predicted

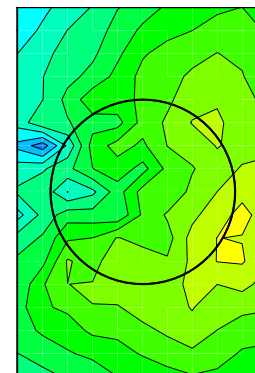


Min Noise

Measured

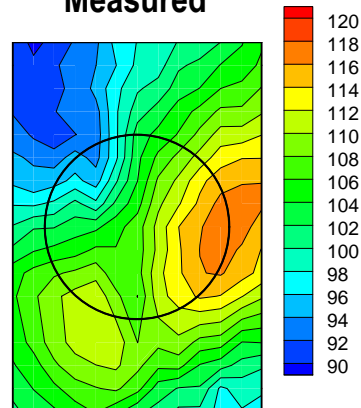


Predicted

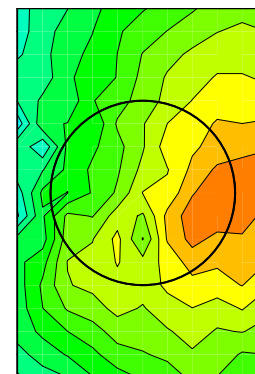


Min Vibration

Measured



Predicted





Issues with Previous Methods

- Fast...
- Loading usually assumed to be compact chordwise.
- Blade motion in acoustics often assumed to be rigid.
 - NOTE: Limitation of data transfer method, NOT of CAMRAD-II or PSU-WOPWOP.
- Isolated rotor... hard to include a fuselage.
- Typically, must “tune” parameters to get good comparisons.

Next... Start looking at couple CFD/CSD method



Work timeline...

Presentation shows results from the following timeframe:

- Winter 2007:
 - Obtained codes: OVERFLOW-DARPA-Y, PSU-WOPWOP v3.3.0, grids, converters
- Spring 2007:
 - Re-grided HART-II blades, grided HART-II sting, coupled cases w/ CAMRAD-II
 - Data Converters re-written for more generality
 - Questioned why there are differences
- Summer/Fall 2007:
 - Cast measured motion into CAMRAD-II variables
 - Began examining possible use of FSC for scattering.
- Winter/Spring 2008:
 - BL, MN, MV cases with “measured” motion.
 - Each with and without the sting in the CFD calculations.
 - Acoustics for all cases.
 - Began porting elastics and co-processing to OVERFLOW 2.1o



Other CFD notes...

- Spalart-Allmaras
- 2nd order dual time stepping w/ Newton subiterations (15 / step)
 - 0.125 degree physical time steps
- 4th order spatial differencing of inviscid terms
- Iterate OVERFLOW until $C_N M^2$ converged.
 - Measured motion cases converged within ~3-4 revs.



Isolated CFD Results: Thrust

OVERFLOW + measured motion

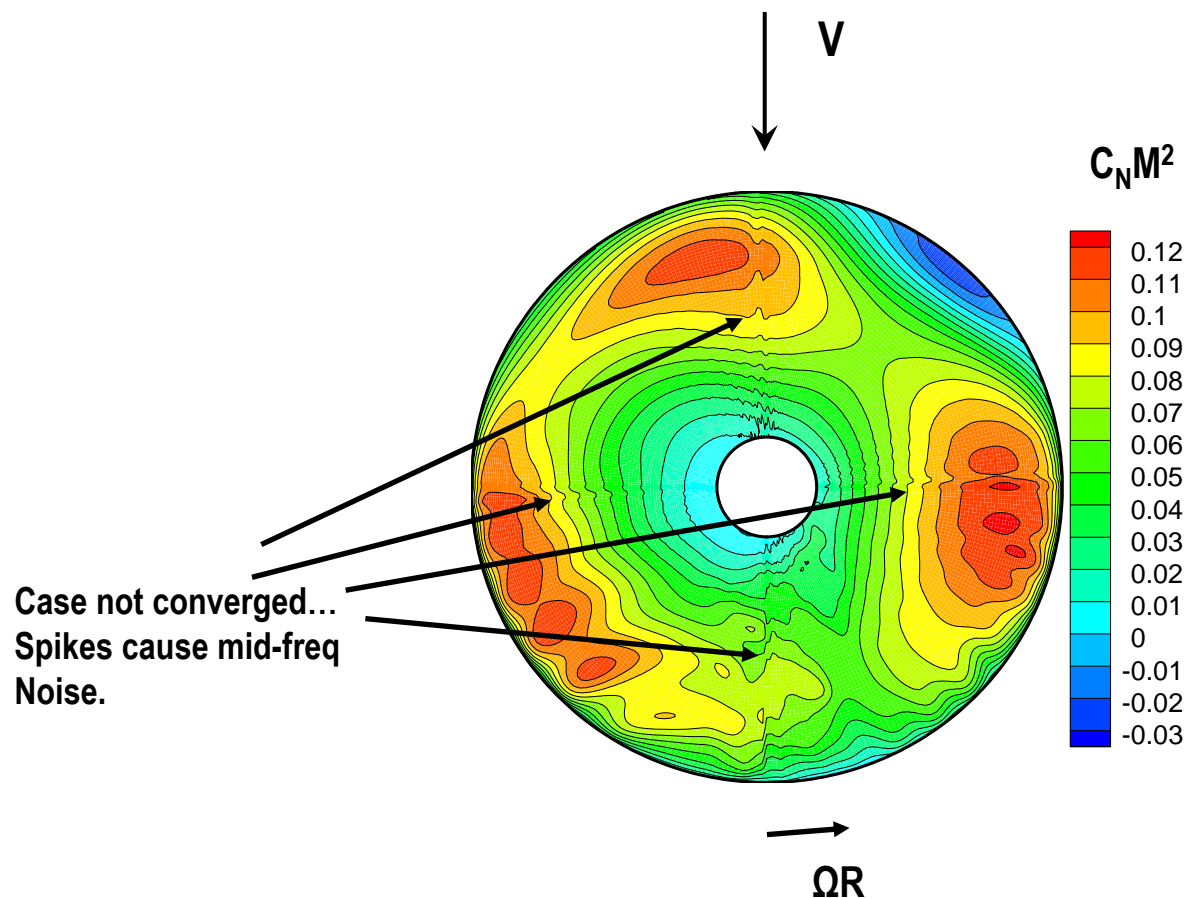
Thrust (Nominal = 3300 N)

Case	Isolated Rotor [N]	Error	Full Configuration [N]	Error
BL	4295	+30%	4318	+31%
MN	4320	+28%	4242	+29%
MV	4339	+31%	4362	+32%

- In all cases, thrust is consistently ~30% over-predicted.
- The reason for this is not yet known.



Min-Vibration Case: Not converged yet.





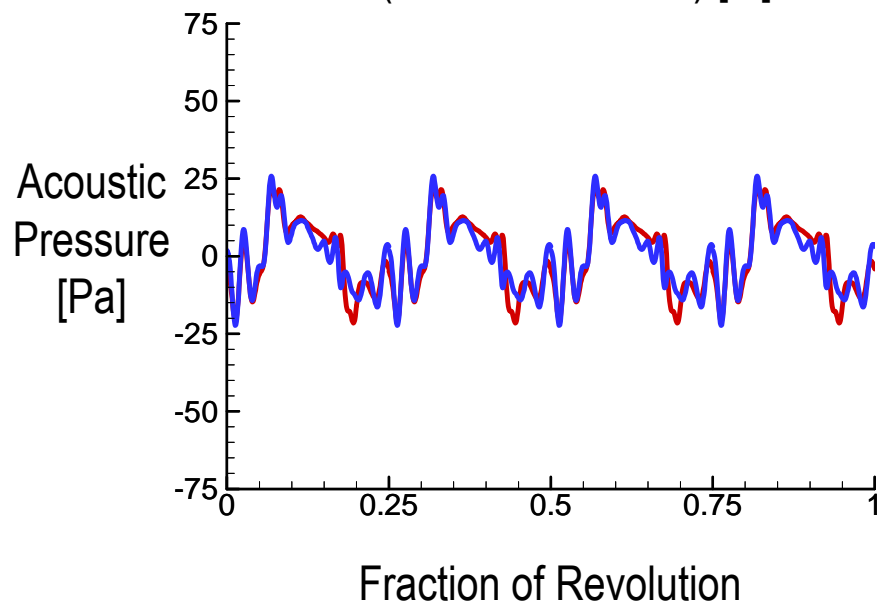
Baseline: Using Measured Motion

Acoustic Pressure Time Histories [Pa]

OVERFLOW + measured motion

— Predicted: Isolated Rotor
— Predicted: Full Configuration

Retreating Side
(2.0, -1.34, -2.215) [m]



Advancing Side
(0.0, 1.81, -2.215) [m]

